Mode Conversion Due To Residual Via Stubs in Differential Signaling

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Motivation

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- Mode conversion is an important degradation cause in differential links.
- Asymmetries on interconnects for differential signaling lead to mode conversion.





Motivation

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• Analysis of a different source of mode conversion: via stub mismatch.

- Back-drilling process can get tolerances of around 10 mil.
- Can asymmetrical via stub length lead to a significant amount of mode conversion?

→ How important is to consider the residual via stubs mismatch in differential signaling?



Contents

- Case of Study
- Mode Conversion Due to Asymmetrical Via Stubs
- Estimation of Mode Conversion as a Function of Residual Via Stub Length
- Conclusions and Outlook
- References

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Case of Study

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- Asymmetrical via stubs are present at the differential Port 01. This can lead to mode conversion!
- Full-wave simulation model.



Case of Study

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- Model has been implemented in an 8-cavity stackup, routed with differential stripline in cavity 2.
- Simulations were validated with FIT and FEM methods.



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Stub effect at the Port 01 (-) results in a timing asymmetry in the differential pair – skew converted into common-mode signals.

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• Important magnitude (~100 mV) of common-mode signals are induced by a stub effect asymmetry!

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• Mode conversion magnitude has a direct relation with the differential via asymmetry.

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• Symmetrical cases (regardless via stub length) present very low mode conversion levels (noise floor)





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- Differences on the differential via stubs in the order of back-drilling residual tolerances can lead to important amount of mode conversion.
- Around 30 GHz, mode conversion can reach a magnitude of around -10 dB.





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- As the frequency increases, magnitude of mode conversion increases as well, reaching high levels for relatively small asymmetries.
- Within the range of typical cavity thicknesses (~10-20 mils), the impact of the stub asymmetry can lead to mode conversion levels up to -25 dB.



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• A low-frequency estimation can be applied, considering the via stub as a shunt capacitor.



Electrical Representation



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• For both sides of the link, there exits residual via stubs:

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• 4-port system can be described in terms of mixed-mode S-parameters.

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-10 • *C_{shunt}* for both sides, can be approximated as: -20 - Sd1c2 [dB] $C \approx \frac{l_{stub}}{v_{ph} \cdot Z_{via}}$ -30 -40 Far-end Mode Conversion -50 **Far-end Mode Conversion** Fundamental Frequency - @2.5 GHz -60 Reference Case [mil] (+) Side (-) Side Method FIT [dB] Estimation [dB] 2 Estimation 4 -70 $\Delta l_{stub} = 22$ -30.33 -31.95 2 8 Estimation $\Delta l_{stub} = 14$ -34.51 -35.86 2 4 FIT -80 $\Delta l_{stub} = 6$ 2 8 FIT -42.11-43.21 $\Delta l_{stub} = 2$ -90 -52.44-52.75 10 50 20 30 40 60 0

Frequency [GHz]



70

• In time domain, this estimation can be reflected as follows:

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Conclusions and Outlook

- Asymmetrical via stubs can be an important source of mode conversion.
- Stub length differences within typical tolerances of back-drilling can induce a maximum mode conversion over -20 dB.
- A low-frequency approximation was used to estimate the amount of mode conversion as a function of the via stub length asymmetry.
- Further investigations can address a comparative analysis against other known sources, e.g. asymmetrical ground via configurations, and the effect of multiple via stub asymmetries.



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- Conclusions and Outlook
- References

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Backup

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• In time domain, this estimation can be reflected as follows:

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